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# Boron doping: B/H/C/O gas-phase chemistry; H atom density dependences on pressure and wire temperature; puzzles regarding the gas-surface mechanism

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#### ABSTRACT

Experimental and modeling studies of the gas-phase chemistry occurring in dilute, hot filament (HF) activated  $B_2H_6/CH_4/H_2$  gas mixtures appropriate for growth of boron-doped diamond are reported. The results of two-dimensional modeling of heat and mass transfer processes and the B/H/C chemistry prevailing in such HF activated gas mixtures (supplemented by reactions involving trace  $O_2$  present as air impurity in the process gas mixture) are discussed and compared with measurements of B atom densities as functions of the hot wire temperature  $T_w$  and distance from the wire. Most of the  $B_2H_6$  molecules that diffuse from the cool, near-wall regions into the hot, near wire region are thermally decomposed (yielding two BH<sub>3</sub> molecules as primary products) and then converted into various 'active' B-containing species like B, BH and BH<sub>2</sub> – some of which are able to accommodate into the growing diamond film. H-shifting reactions BH<sub>x</sub> + H  $\leftrightarrow$  BH<sub>x-1</sub> + H<sub>2</sub> enable rapid inter-conversion between the various BH<sub>x</sub> (x=0-3) species and the BH<sub>x</sub> source is limited by diffusional transfer of  $B_2H_6$ . H atoms play several key roles – *e.g.* activating the process gas mixture, and gas pressure dependences of the H atom production rate (by H<sub>2</sub> dissociation on the HF surface) can be accommodated by a simple gas-surface reaction model.

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#### 1. Introduction

Hot-filament (HF) activation of dilute hydrocarbon/ $H_2$  (e.g.  $CH_4/H_2$ ) gas mixtures is an established low-cost route for diamond chemical vapour deposition (CVD) [1–3]. Addition of trace amounts of a boron containing precursor (e.g. 10-1000 ppm of B<sub>2</sub>H<sub>6</sub>) during diamond CVD is of considerable interest, as incorporated B atoms act as acceptors  $(E_a \sim 0.37 \text{ eV})$  and impart p-type semiconductivity to the as-grown Bdoped diamond [4]. B-doped diamond is attracting interest for its potential application in electronic and optical devices [5,6], bio-sensing [7], and as a result of its more recently discovered superconductivity [8,9]. All such applications require reliable recipes for forming high quality B-doped diamond, with controllable doping levels; hence the emerging need for a much fuller understanding of the doping processes and of the B/H/C chemistry. However, the details of the gas-phase and gas-surface chemistry involved in the growth of B-doped CVD diamond are still poorly understood. The literature contains only a handful of papers reporting diagnostics relevant to B-containing microwave (MW) plasmas, though several studies have sought to establish relationships between diamond film quality, dopant concentration and reactor parameters such as the B<sub>2</sub>H<sub>6</sub> flow rate (or the input [B]/[C] ratio), substrate temperature, etc. [10-12]. We have embarked on combined

#### 2. Modeling of HFCVD reactor processes in B/H/C/O mixtures

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To start the study of B/H/C/(O) chemistry in HFCVD reactors one first needs to be able to describe the processes involved in diamond

experimental and theoretical studies of the B/H/C chemistry prevailing in both HFCVD [13] and MW plasma enhanced (PE) CVD reactors [14,15]. The experimental part of the HFCVD project has involved use of resonance enhanced multiphoton ionization (REMPI) techniques to measure spatially resolved relative number densities of B (and H) atoms - henceforth represented as [B], [H], etc. - as functions of process conditions (e.g. the hot wire material, and its temperature  $T_w$ , gas pressure p, the  $B_2H_6/H_2$  mixing ratio, and the presence (or not) of added CH<sub>4</sub>) [13]. The complementary modeling builds on previous analyses of CH<sub>4</sub>/H<sub>2</sub> [3,16–18], CH<sub>4</sub>/NH<sub>3</sub>/H<sub>2</sub> [19], B<sub>2</sub>H<sub>6</sub>/H<sub>2</sub> and CH<sub>4</sub>/B<sub>2</sub>H<sub>6</sub>/H<sub>2</sub> [13] gasphase and gas-surface chemistry in HFCVD reactors. One of the challenges of the present study is to determine the important reaction pathways (with known and/or assumed rate coefficients) in B/C/H gas mixtures under typical HFCVD reactor conditions. Our recent studies of B/H/C chemistry in a MW PECVD reactor [14,15] showed that trace amounts of O<sub>2</sub> impurity (air leakage, impurity in source gas) present at concentrations comparable to the B<sub>2</sub>H<sub>6</sub> concentrations typically used in B-doped diamond CVD can have a major effect on the BH<sub>x</sub> concentrations - hence the need to establish the much more complex, four component, B/H/C/O chemical mechanism.

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deposition from conventional (*e.g.* 1%CH<sub>4</sub>/H<sub>2</sub>) mixtures, *i.e.* proper treatments of the catalytic dissociation of H<sub>2</sub> on the HF surface, the H/C gas-phase chemistry, the gas temperature ( $T_{gas}$ ) and species concentration distributions, diamond growth models, *etc.* Then one needs to collect and analyze scarce data on B/H/O chemical kinetics and thermochemistry from previous studies under conditions that, as a rule, are far from the typical HFCVD conditions. These include combustion studies of boranes ( $B_xH_y$ ) in the search for high-energy fuels [20–22], studies of MW PECVD reactors [14,15,23,24], theoretical studies of various  $B_xH_y$ ,  $B_xH_yO_z$  species, their structures and reactions with H, H<sub>2</sub>, H<sub>x</sub>O<sub>y</sub> and C<sub>x</sub>H<sub>y</sub> species [20–22,25,26], and B<sub>2</sub>H<sub>6</sub> dissociation studies (in B<sub>2</sub>H<sub>6</sub> and B<sub>2</sub>H<sub>6</sub>/H<sub>2</sub> mixtures) [27]. Below we describe the main stages of our model development.

#### 2.1. Catalytic H<sub>2</sub> dissociation on HF surface

H atoms play a crucial role in activating the process gas mixtures and initiating the various inter-conversions within and between the  $CH_x$  and  $C_2H_y$  families (and  $H_xB_yC_zO_{z'}$  species in B/H/C/O mixtures). Previous theoretical [16,18,28,29] and experimental studies have explored H atom densities (as functions of process parameters) by, for example, REMPI [3,13], laser induced fluorescence [30], thirdharmonic generation [31], and calorimetric studies of the filament power balance in order to establish the fractions of supplied electrical power expended through radiation, conduction and catalytic H<sub>2</sub> dissociation [18,32,33]. Such studies have shown that the distribution of H atom densities under typical HFCVD reactor conditions (e.g.  $p \sim 10-50$  Torr,  $T_w \sim 2300-2700$  K) is largely established by the balance of production (H<sub>2</sub> catalytic dissociation on the HF surface), loss (both recombination on the cold reactor walls, substrate, substrate holder, and consumption in gas-phase reactions) and diffusional transfer. The H atom source term should be well described as a function of process parameters like p and  $T_w$ , but various aspects of the dissociation mechanism and measured dependences remain unclear. For example, the input powers required to maintain the hot wire at a given  $T_w$ appear to saturate at  $p(H_2) \sim 10-20$  Torr, as do the measured H atom concentrations (which thereafter remain flat or even decline slightly upon increasing  $p \sim 100$  Torr) – in marked contradiction with expectations based on the ~5-fold increase of the number of collisions between H<sub>2</sub> molecules and the HF surface and the ~5-fold decrease in the diffusional coefficient  $(D \sim 1/p)$  [18]. In addition,  $T_w$  dependent measurements of the effective enthalpy for forming H atoms return a value,  $\Delta H \sim 2.45$  eV, that is much lower than the H<sub>2</sub> bond strength [18]. In an attempt to explain such apparent paradoxes, we recently proposed a self-consistent approach based on analytical distributions of  $T_{gas}$  and H atom concentrations in the immediate proximity of the HF, and a simple gas-surface model based on two effective (and reversible) chemisorption/desorption reactions:

$$S^{*} + H_{2} \leftrightarrow SH + H, \qquad k_{1} \left[ cm^{3}/s \right] = 2.8 \times 10^{-12} T_{nw}^{0.5} \exp(-10440 / T_{w}), \qquad (1)$$

$$k_{-1} = 1.5 \times 10^{-11} \left[ cm^{3}/s \right]$$

$$SH \leftrightarrow S^{*} + H, \qquad k_{2} \left[ s^{-1} \right] = 10^{13} \exp(-41780 / T_{w}), \qquad (2)$$

$$k_{-2} = 2.85 \times 10^{-11} \left[ cm^{3}/s \right].$$

S<sup>\*</sup> and SH are the active (free) and H-terminated sites on the HF surface, respectively,  $[S_0] = [SH] + [S^*]$  is the total surface site density per unit area,  $T_{nw} = T_{gas}(d=0)$  is the gas temperature adjacent to the hot wire surface, *d* is the distance from the HF, and  $k_i$  are the rate coefficients adopted in [18] for a bare Ta wire. This approach affords a consistent description of all of the experimental observations, and the measured trends upon varying *p* and  $T_w$ . In particular, the saturation of the catalytic source term Q [cm<sup>-2</sup> s<sup>-1</sup>] (where Q is the number of H atoms produced

per second per unit area of hot surface, *i.e.*  $Q = 2(R_1 - R_{-1}) = 2(R_2 - R_{-2})$ in terms of reaction rates  $R_i$  (i=1, 2) [18]) and of the H atom densities measured a few mm from the HF surface are explained by the appropriate drop of the free site fraction  $[S^*]/[S_0]$  – as can be seen in Fig. 1, which illustrates results from [18] for the case of a bare Ta wire at  $T_w = 2440$  K in  $H_2$  gas. This plot also highlights the sensitivity of the [H](d=2 mm)/[H](d=0) ratio to  $p(H_2)$ : the observed saturation of the H atom density measured a few mm from the HF surface does not imply a similar saturation for the H atom concentration at d=0. This effect, which is induced by the very steep gradients in  $T_{gas}$  and [H] near the HF [18] and the decline in the diffusion coefficient with  $p(D_{\rm H} \sim 1/p)$ , illustrates a limitation of using H atom concentrations measured near the HF as a proxy for the H atom densities at the HF surface itself when varying  $p(H_2)$ : such an assumption introduces a >200% error in the [H](d=2 mm)/[H](d=0)ratio across the range  $20 < p(H_2) < 100$  Torr. The catalytic source term Q is an important parameter for the 2D/3D models discussed below.

#### 2.2. 2D/3D models of HFCVD reactor processes

Another important element in our theoretical studies is the development of 2D(r,z) and 3D(x,y,z) models to describe (i) activation of the reactive mixture (e.g. gas heating, catalytic H atom production on the HF and, in the present case, loss of gas-phase boron by incorporation at the HF surface), (ii) gas-phase processes (heat and mass transfer, and chemical kinetics), and (iii) gas-surface processes at the substrate. The models involve the conservation equations for mass, momentum, energy, and species concentrations, together with appropriate initial and boundary conditions, thermal and caloric equations of state. These equations are integrated numerically to yield spatial distributions of  $T_{gas}$ and, in the case of H/C gas mixtures, the various  $H_xC_y$  species (H, H<sub>2</sub>,  $CH_x$ (x=0-4), C<sub>2</sub>H<sub>v</sub>(y=0-6)) densities. The calculated results for different reactor parameters succeed in reproducing a wealth of data and trends observed experimentally [3,16–19]. For the present study of B-doped diamond deposition, the chemical mechanism was necessarily expanded to incorporate the B/H/C/O mechanism described below.

Most of the calculations in the present study employed the computationally less time consuming 2D(r,z) model and base conditions as follows: p = 20 Torr, substrate temperature  $T_{sub} = 1073$  K, flow rates  $F(CH_4) = 1$  standard cm<sup>3</sup> per minute (sccm),  $F(H_2) = 99$  sccm,  $F(B_2H_6) = 0.0475$  sccm, and  $T_w$  values of 2073, 2300 and 2573 K. The reactor is represented in cylindrical coordinates, with *z* parallel to the direction of gas flow. The modeling considers a part of the Bristol HFCVD reactor (a chamber based on a six-way cross). The model reactor volume was bounded in the radial and vertical directions by, respectively, 0 < r < 25 mm and -10 mm < z < 30 mm, with the point (0,0) defining



**Fig. 1.** Plot illustrating the calculated  $p(H_2)$  dependences of the catalytic H atom production rate *Q*, the free site fraction [S<sup>\*</sup>]/[S<sub>0</sub>] and the [H](d=2 mm)/[H](d=0) ratio for a bare Ta HW at  $T_w = 2440 \text{ K}$ .

the center of the substrate. The assumed cylindrical symmetry offers, at best, an approximate representation of the location and volume of the experimental Ta (Re) HF (0.250 mm diameter, 7 turns with coil diameter ~3 mm and coil length ~8 mm, providing a geometrical hot surface area  $S_{hot} \sim 0.57 \text{ cm}^2$ ). In the model, the HF volume was confined within the cylinder r < 2 mm, 10 < z < 13 mm. The temperature drop  $\Delta T = T_w - T_{gas}(d=0) \sim 250$  K between the HF surface and the immediate gas phase was estimated using the Smoluchowski formula and an H<sub>2</sub> accommodation coefficient ~0.3-0.4 [34]. Estimates for the catalytic H atom production rates  $Q(T_w)$  per cm<sup>2</sup> of the HF surface were taken from previous data [13,18,19], yielding the effective enthalpy  $\Delta H \sim 2.18 \text{ eV}$ for borodized Ta (*i.e.* TaB) wires at T<sub>w</sub><2400 K and the decline of H atom concentration at  $T_w$ >2400 K [35]. H atom production rates  $Q(T_w, TaB)$  $\sim$ 9 $\times$ 10<sup>18</sup>, 3 $\times$ 10<sup>19</sup> and 4.85 $\times$ 10<sup>19</sup> cm<sup>-2</sup> s<sup>-1</sup> were used here for borodized Ta wires at  $T_w = 2073, 2300$  and 2573 K, respectively, and  $Q(T_w, TaCB) = Q$ (Tw,TaB)/2 for carburized-borodized Ta wires in B/H/C mixtures. The substrate and substrate holder located at (r < 1 mm, -10 < z < 0 mm) in the present modeling was chosen to have minimal radius (i.e. 1 mm, which is the grid cell size in both the r and z directions) simply to retain the possibility of calculating species densities just above the substrate surface (r < 1 mm, z = 0) and thus to compare with the B atom profiles measured experimentally in the absence of any substrate and substrate holder. The regions (r < 3 mm, z = 30 mm) and (23 < r < 25 mm, z = -10 mm) define the gas inlet and outlet positions in the model,  $T_{sub}$ was kept constant (at 1073 K) and  $T_{gas}$  at the reactor walls was set to 300 K.

#### 2.3. B/H/C/O chemical mechanism

The available chemical and thermochemical data for B-containing species together with our recent thorough experimental and theoretical study of MW activated B<sub>2</sub>H<sub>6</sub>/Ar/H<sub>2</sub> [14] and B<sub>2</sub>H<sub>6</sub>/CH<sub>4</sub>/Ar/H<sub>2</sub> [15] plasmas used for CVD of B-doped diamond have allowed development of a B/H/C/O chemical mechanism and its testing on a variety of experimental measurements [14,15]. Briefly, the absolute column densities of ground state B atoms, electronically excited H(n=2)atoms, and BH, CH and C2 radicals in MW activated B/H/C/Ar plasmas have been determined by cavity ring down spectroscopy, as functions of process conditions. Optical emission spectroscopy has also been used to explore variations in the relative densities of electronically excited H atoms, H<sub>2</sub> molecules and BH, CH and C<sub>2</sub> radicals. These experimental data have been complemented by extensive 2D(r,z) modeling of the plasma chemistry, and have enabled substantial refinements to the existing B/H/ C/O thermochemistry and chemical kinetics. The combined experimental/2D modeling study indicates that deposition of B-containing material on the reactor walls (mainly from B atom adsorption, with some participation from H<sub>2</sub>O) becomes progressively less important at higher  $F(CH_4)$  [15]. B/H/C/(O) coupling reactions are deduced to play important (but still incompletely understood) roles in determining the local BH<sub>x</sub> (x=0-3) number densities. Most (75–80%) of the B<sub>2</sub>H<sub>6</sub> in the input gas mixture is efficiently dissociated in the hot plasma and near plasma regions, at gas temperatures  $T_{gas}$  > 1000 K [15]. The resulting BH<sub>x</sub> species undergo further processing, and much of the boron is deduced to be stored as more stable  $H_x B_y C_z O_{z'}$  reservoir species like HBO,  $H_2 BO$ , H<sub>3</sub>COBH<sub>2</sub> and, particularly, CH<sub>2</sub>CHBH<sub>2</sub> and CH<sub>3</sub>CH<sub>2</sub>BH<sub>2</sub>. The spatial profiles of the various BH<sub>x</sub> species reflect the complex balance of diffusional transfer and inter-conversions between the various families of B-containing species in the different local environments  $(T_{gas}, [H], [H_2O], [C_xH_y], etc.)$ . Key conversions in the mechanism proposed here include  $BH_x \leftrightarrow H_y BC_z$  (involving  $C_2 H_2$  and  $C_2 H_4$ ) and  $BH_x \rightarrow H_v BO \rightarrow H_z COBH_v \rightarrow BH_x$  (via reactions with, or activation by,  $H_2O$ ,  $CH_x$  species and/or H atoms).

These refined B/H/C and B/H/C/O mechanisms were embedded in the existing 2D(r,z) and 3D(x,y,z) models of a HFCVD reactor to determine the important reaction pathways under typical HFCVD reactor conditions. The B/H/C chemical kinetics mechanism employed includes 112 direct and reverse reactions for 23 species (H, H<sub>2</sub>, CH<sub>x</sub> (x=0-4), C<sub>2</sub>H<sub>y</sub>(y=0-6), BH<sub>x</sub>(x=0-3), B<sub>2</sub>H<sub>6</sub>, CH<sub>2</sub>CHBH<sub>2</sub> and CH<sub>3</sub>-CH<sub>2</sub>BH<sub>2</sub>). As mentioned above, trace amounts of O<sub>2</sub> impurity (from air leakage, and/or as an impurity in the source gas) at number densities comparable to the typical B<sub>2</sub>H<sub>6</sub> concentrations can have a serious impact on the BH<sub>x</sub> species concentrations. To trace such effects of oxygen, additional conversions involving HBO, H<sub>2</sub>BO, O<sub>2</sub>, O, OH, H<sub>2</sub>O, CO, H<sub>x</sub>CO, H<sub>x</sub>CCO, x=1,2, and H<sub>x</sub>COBH<sub>2</sub> (x≤3) species have been introduced in the full B/H/C/O chemical mechanism, which includes 276 direct and reverse reactions.

## 3. Calculated results: B/H/C/(O) chemistry in HFCVD reactor conditions

All aspects of the deceptively simple HFCVD reactor processes described above were incorporated in the 2D(r,z) model for simulating the B-doped diamond deposition process. Armed with such a model, we can predict spatial distributions of hydrogen, hydrocarbon and B-containing species in the Bristol HFCVD reactor, for comparison with measured B atom profiles and their dependence on  $T_{w}$ , distance *d* from the HF and CH<sub>4</sub> fractions (0 or 1%). The observation that [B] doubles when *F*(CH<sub>4</sub>) was reduced to zero forced us to introduce an additional diborane dissociation channel involving





**Fig. 2.** Calculated 2D(*r*,*z*) distributions of a) the  $T_{gas}$  (left half-panel) and the H atom mole fraction  $X_{H}$ , and b) the B atom (left half-panel) and  $B_2H_6$  concentrations for 0.0475% $B_2H_6/1$ %CH<sub>4</sub>/H<sub>2</sub> mixture,  $T_w$ =2300 K and p=20 Torr. The substrate holder and the HW volume (rectangular mesh at the image center) assumed in the modeling are indicated also. The model reactor volume was bounded in the radial and vertical directions by, respectively, 0 < r < 25 mm and -10 mm < z < 30 mm, the point (0,0) is the center of the substrate.



**Fig. 3.** a) Plots of [B] vs *d* using a borodized Ta HW, measured in 0.0475%B<sub>2</sub>H<sub>6</sub>/H<sub>2</sub> mixture at the specified  $T_w$  values. The superposed lines through the data are intended merely to guide the eye. b) Plots of calculated [B] vs *d* for 0.0475%B<sub>2</sub>H<sub>6</sub>/x%CH<sub>4</sub>/H<sub>2</sub> (x = 0 or 1) mixtures and  $T_w = 2073$ , 2300 and 2573 K assuming B atom loss probability on the wire surface  $\gamma_W = 0$  or  $\gamma_W = 1$  (for  $T_w = 2573$  K).

reaction with H atoms, *i.e.*  $B_2H_6 + H \rightarrow BH_4 + BH_3 \rightarrow 2BH_3 + H$ . The total  $B_2H_6$  decomposition rate was thus described as follows,

$$B_2H_6 + M \rightarrow BH_3 + BH_3 + M, \ k[cm^3 s^{-1}] = 4.2 \times 10^{-7} exp(-17008 / T_{gas})$$
 (3)

with  $M = B_2H_6$  (enhancement factor = 1),  $C_2H_2$  (0.1),  $CH_4$  (0.1), H (0.05). Test calculations assuming various different probabilities,  $\gamma_{B_2H_6}$ , for the catalysed decomposition of  $B_2H_6$  on the HF surface indicate that this process might make a contribution to BH<sub>3</sub> production comparable to that from thermal dissociation only at low  $T_w$  and high  $\gamma_{B_2H_6}$  (e.g. surface catalysed dissociation might contribute ~50% of the total BH<sub>3</sub> production rate at  $T_w = 2073$  K and  $\gamma_{B_3H_6} = 0.5$ ).

The results of the 2D modeling in the 0.0475%B<sub>2</sub>H<sub>6</sub>/1%CH<sub>4</sub>/H<sub>2</sub> mixture are illustrated by the 2D(*r*,*z*) distributions of  $T_{gas}$ , the H atom mole fraction, and the B atom and B<sub>2</sub>H<sub>6</sub> number densities shown in Fig. 2a and b, respectively, for  $T_w = 2300$  K. Most of the B<sub>2</sub>H<sub>6</sub> molecules that diffuse from the cool, near-wall regions into the hot, near HF region are thermally decomposed, giving two BH<sub>3</sub> molecules as primary products, which are then further converted into 'active' B-containing species like B, BH and BH<sub>2</sub> — some of which are able to accommodate into the growing diamond film and at the reactor walls. The H-shifting reactions BH<sub>x</sub> + H  $\leftrightarrow$  BH<sub>x-1</sub> + H<sub>2</sub> enable rapid inter-conversion between the various BH<sub>x</sub> (x = 0-3) species, favoring B atoms in the wire–substrate gap; the BH<sub>x</sub> source is seen to be limited by diffusional transfer of B<sub>2</sub>H<sub>6</sub>. The

#### Table 1

Species concentrations [cm<sup>-3</sup>] above the substrate (at r=0, z=0.5 mm) for  $0.01\%B_2H_6/$  $0.01\%O_2/1\%CH_4/H_2$  mixture ( $T_w=2300$  K,  $\gamma_W=0$ ) and  $0.0475\%B_2H_6/1\%CH_4/H_2$  mixtures  $T_w=2300$  ( $\gamma_W=0$ ) and 2573 K ( $\gamma_W=1$ ). The number format 6.05E + 14 stands for  $6.05 \times 10^{14}$ . The last row shows the estimated diamond growth rate, *G*, in µm/h.

T <sub>w</sub> /K	2300	2300	2573
Н	6.03E+14	6.05E+14	7.93E+14
CH₃	1.49E+13	1.49E+13	2.45E+13
C <sub>2</sub> H <sub>2</sub>	6.54E+12	5.40E+12	1.72E+13
CH <sub>2</sub>	4.73E+09	4.75E+09	1.26E+10
$CH_2(S)$	8.23E+07	8.27E+07	2.17E+08
СН	1.02E+08	1.02E+08	3.52E+08
С	3.18E+08	3.21E+08	1.92E + 09
C <sub>2</sub> (a)	3.00E+07	2.99E+07	2.32E+08
$C_2(X)$	5.28E+04	5.27E+04	4.64E + 05
C <sub>2</sub> H	1.70E+05	1.44E+05	9.19E+05
C <sub>2</sub> H <sub>6</sub>	1.90E+12	2.01E+12	2.34E+12
$C_2H_4$	1.64E+12	1.58E+12	3.10E+12
C <sub>2</sub> H <sub>5</sub>	8.12E+09	8.50E+09	1.19E+10
C <sub>2</sub> H <sub>3</sub>	1.36E+10	1.18E+10	3.38E+10
$B_2H_6$	5.59E+12	2.69E+13	2.09E+13
BH <sub>3</sub>	8.88E+10	3.45E+11	1.52E + 11
BH <sub>2</sub>	3.86E+08	1.50E+09	9.18E+08
BH	5.78E+08	4.60E+09	4.54E + 09
В	1.07E+11	1.73E+12	1.76E+12
CHCH <sub>2</sub> BH <sub>2</sub>	2.96E+11	8.06E+11	7.92E+11
CH <sub>2</sub> CH <sub>3</sub> BH <sub>2</sub>	6.08E+10	2.39E+11	1.61E + 11
CH4	9.41E+14	9.41E+14	8.92E + 14
H <sub>2</sub>	1.97E+17	1.97E+17	1.93E+17
H <sub>x</sub> BO	4.08E+12		
02	2.22E+12		
H <sub>2</sub> O	3.99E+12		
CO	9.55E+11		
2 F(B <sub>2</sub> H <sub>6</sub> )/F(CH <sub>4</sub> )	0.02	0.1	0.1
[B]/[CH <sub>3</sub> ]	0.007	0.12	0.07
G, μm/h	0.16	0.16	0.26

calculations show that B atom loss at the reactor walls affects both the absolute concentrations of the various  $BH_x$  species, and their profiles.

Comparison between Fig. 3a and b shows that the modeling reproduces the B atom spatial profiles observed with the 0.0475%  $B_2H_6/H_2$  mixture well if we assume a probability of B atom loss at the wall,  $\gamma_{\text{wall}} = 0.1$  [13]. The general decline in [B] at large *d* can be reproduced with smaller  $\gamma_{wall}$  values also, but all calculations with  $\gamma_{\text{wall}} = 0$  return [B] profiles which increase with increasing d. The modeling fails to replicate the observed fall in [B] at  $T_{\rm W}$ >2350 K but, as previously [13], the measured fall can be reproduced reasonably well by assuming a marked increase in the loss probability  $\gamma_w$  of B atoms at the HF surface at temperatures that exceed the melting temperatures of boron ( $T_{mp}$ ~2350 K) and TaB ( $T_{mp}$ ~2313 K). As an illustration of this effect, Fig. 3b shows the B atom concentration at  $T_w = 2573$  K calculated assuming  $\gamma_w = 1$ . The last two curves in Fig. 3b, for the case of a 0.0475%  $B_2H_6/1\%CH_4/H_2$  mixture with  $T_w = 2300$  K,  $\gamma_w = 0$  and  $T_w = 2573$  K,  $\gamma_{\rm w} = 1$ , respectively, successfully mimic the experimentally observed [13] fall in [B] at d = 3 mm upon introducing  $F(CH_4) = 1$  sccm.

Preliminary calculations exploring the effect of O<sub>2</sub> impurity (at concentrations of 100 ppm, much less than the 500 ppm of B<sub>2</sub>H<sub>6</sub> assumed in our base conditions) show conversion of BH<sub>x</sub> species to H<sub>y</sub>BO(y = 1,2) species (mainly through the reaction of B atoms with H<sub>2</sub>O), but the B atom densities are only reduced seriously once  $F(O_2)$  approaches  $F(B_2H_6)$ . Thus, we here focus on presenting the calculated species distributions above the substrate surface for the specific cases of a 0.01%B<sub>2</sub>H<sub>6</sub>/0.01%O<sub>2</sub>/1%CH<sub>4</sub>/H<sub>2</sub> mixture (*i.e.*  $F(B_2H_6) = F(O_2)$ ) at  $T_w = 2300$  K and an O<sub>2</sub>-free 0.0475%B<sub>2</sub>H<sub>6</sub>/1%CH<sub>4</sub>/H<sub>2</sub> mixture at  $T_w$  values of 2300 and 2573 K. Table 1 shows the calculated species concentrations at r = 0, z = 0.5 mm for these three sets of conditions. Inspection of these data clearly illustrates the reduction in [B] induced by the presence of O<sub>2</sub> (*i.e.* [B](column 1)<[B](column 2)/4.75 (because [B]~ $F(B_2H_6)$  for the O<sub>2</sub>-free case). Given these densities, we can also estimate the diamond growth rate *G* which, under these conditions, will

be dictated by the incident density of CH<sub>3</sub> radicals. The growth rate was estimated from the formula [36,37]

$$G = 0.075 \times 3.8 \times 10^{-14} T_{\text{sub}}^{0.5} [\text{CH}_3] / \{1 + 0.3 \cdot \exp(3430 / T_{\text{sub}})$$
(4)

$$+ 0.1 \exp(-4420 / T_{sub})[H_2] / [H]\}.$$

The predicted [B]/[CH<sub>3</sub>] number density ratio at a growing diamond surface (~0.07–0.12) is close to  $2 F(B_2H_6)/F(CH_4) \approx 0.1$  for the O<sub>2</sub>-free cases. For a reliable estimation of the likely B incorporation rate a more detailed simulation employing the full-scale HFCVD reactor geometry and experimental characterization of B-doping level would be required. At this stage, the present modeling only allows us to conclude that B-doping of CVD diamond in HFCVD reactors is likely to be provided by B atoms, which are the dominant BH<sub>x</sub> species near the substrate and the HF.

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